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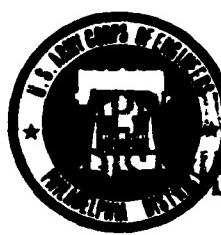
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DELAWARE RIVER BASIN  
BEAVER BROOK, WARREN COUNTY  
NEW JERSEY

# HOPE LAKE DAM NJ 00796

PHASE 1 INSPECTION REPORT  
NATIONAL DAM SAFETY PROGRAM



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DEPARTMENT OF THE ARMY

Philadelphia District  
Corps of Engineers  
Philadelphia, Pennsylvania

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report. → pg. 1		



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21 AUG 1981

Honorable Brendan T. Byrne  
Governor of New Jersey  
Trenton, New Jersey 08621

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Hope Lake Dam in Warren County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Hope Lake Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in very poor overall condition. The dam's spillways are considered inadequate because a flow equivalent to 5 percent of the Spillway Design Flood (SDF) would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated. In the interim, during periods of unusually heavy precipitation, around the clock surveillance should be provided.

b. Within three months from the date of approval of this report the owner should engage a qualified professional consultant to perform the following:

(1) Investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam.

(2) Design procedures for and inspect the removal of the trees and their roots from the entire embankment.

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Honorable Brendan T. Byrne

- (3) Design procedures for and inspect the construction of erosion protection on the upstream slope of the dam.
  - (4) Design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place.
  - (5) Design channels to reroute the flowing water away from the toe of the dam.
  - (6) Establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway.
- c. Within one year from the date of approval of this report the owner should engage a qualified professional consultant to design and supervise installation of adequate means to drain the reservoir in case of emergency.
- d. Within thirty days from the date of approval of this report the following remedial actions should be initiated:
- (1) Clear debris and trees from the spillway discharge channels and maintain the channels free from debris.
  - (2) Clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris.
  - (3) Clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways.
- e. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.
- f. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Courter of the Thirteenth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

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Honorable Brendan T. Byrne

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,



1 Incl  
As stated

ROGER L. BALDWIN  
Lieutenant Colonel, Corps of Engineers  
Commander and District Engineer

Copies furnished:

Mr. Dirk C. Hofman, P.E., Deputy Director  
Division of Water Resources  
N.J. Dept. of Environmental Protection  
P.O. Box CN029  
Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief  
Bureau of Flood Plain Regulation  
Division of Water Resources  
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P.O. Box CN029  
Trenton, NJ 08625

HOPE LAKE DAM (NJ00796)

CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 21 April 1981 by Anderson-Nichols and Co. Inc., under contract to the State of New Jersey. The State, under agreement with the U.S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92-367.

Hope Lake Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in very poor overall condition. The dam's spillways are considered inadequate because a flow equivalent to 5 percent of the Spillway Design Flood (SDF) would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated. In the interim, during periods of unusually heavy precipitation, around the clock surveillance should be provided.

b. Within three months from the date of approval of this report the owner should engage a qualified professional consultant to perform the following:

(1) Investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam.

(2) Design procedures for and inspect the removal of the trees and their roots from the entire embankment.

(3) Design procedures for and inspect the construction of erosion protection on the upstream slope of the dam.

(4) Design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place.

(5) Design channels to reroute the flowing water away from the toe of the dam.

(6) Establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway.

c. Within one year from the date of approval of this report the owner should engage a qualified professional consultant to design and supervise installation of adequate means to drain the reservoir in case of emergency.

d. Within thirty days from the date of approval of this report the following remedial actions should be initiated:

(1) Clear debris and trees from the spillway discharge channels and maintain the channels free from debris.

(2) Clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris.

(3) Clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways.

e. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

f. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

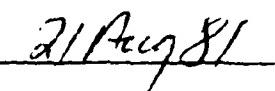
APPROVED:



ROGER L. BALDWIN

Lieutenant Colonel, Corps of Engineers  
Commander and District Engineer

DATE:



PHASE I INSPECTION REPORT  
NATIONAL DAM SAFETY PROGRAM

Name of Dam:	Hope Lake
Identification No.:	Fed ID No. NJ00796
State Located:	New Jersey
County Located:	Warren
Stream:	Beaver Brook
River Basin:	Delaware
Date of Inspection	April 21, 1981

ASSESSMENT OF GENERAL CONDITIONS

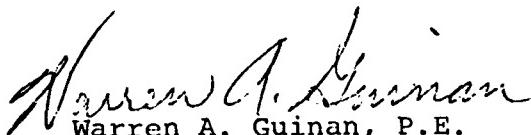
Hope Lake Dam is an earthfill, stone masonry, and concrete dam, about 200 years old, that is in poor overall condition. It is small in size and should be downgraded to significant hazard from its initial classification of high hazard. Trees and brush are growing on both upstream and downstream slopes of the earth embankment portions of the dam. One large tree has blown down causing a large hole in the downstream embankment where the roots were torn out near the left abutment of the principal spillway. Severe erosion of the embankments on either side of the stoplog spillway has undermined the concrete capping and exposed the concrete and stone masonry of the training walls. Much of the downstream stone masonry face under the concrete apron of the emergency spillway has collapsed leaving the slab unsupported. Erosion of the upstream slope at and above the waterline has occurred. Soft, wet areas were noted along the downstream toe of the embankment portions with some clear water discharges. The left abutment of the principal spillway has been patched; yet some leakage was noted below the patch. Leakage around the ends and through the stoplogs was observed. Also, seepage is occurring through the upstream concrete or stone masonry faces at both the stoplog and emergency spillways. The total combined capacities of the principal, emergency, and stoplog spillways (with stoplogs in place) can pass 4 percent of the one-half PMF without overtopping; thus the spillways are considered inadequate.

It is recommended that the owner retain the services of a professional engineer, qualified in the design and inspection of dams, to accomplish the following in the time periods specified. Starting immediately: investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam; very soon: design procedures for and inspect the removal of the trees and their roots from the entire embankment; design procedures for and inspect the construction of erosion

protection on the upstream slope of the dam; design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place; design channels to reroute the flowing water away from the toe of the dam; and establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway. In the near future: further evaluate the hydrology and hydraulics of the watershed, reservoir, dam, spillways, and design and implement remedial measures; and design and install adequate means to drain the reservoir in case of emergency.

It is also recommended that, as a part of operating and maintenance procedures, the owner should immediately clear debris and trees from the spillway discharge channels and maintain the channels free from debris; check the condition of the dam periodically; clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris, and clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways. In addition, in the future: establish a surveillance program for use during and immediately following periods of heavy rainfall and also a warning program to follow in case of emergency conditions.

ANDERSON-NICHOLS & COMPANY, INC.



Warren A. Guinan, P.E.  
Project Manager  
New Jersey No. 16848

21 April 1981

OVERVIEW  
HOPE LAKE DAM



## PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonable possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT  
NATIONAL DAM SAFETY INSPECTION PROGRAM  
HOPE LAKE DAM  
FED ID NO. #NJ00796

SECTION 1  
PROJECT INFORMATION

5.1 General

a. Authority. Authority to perform the Phase I Safety Inspection of Hope Lake Dam was received from the State of New Jersey, Department of Environmental Protection, Division of Water Resources by letter dated 12 December 1980 under Basic Contract No. FPM-39 and Contract No. A01093 dated 10 October 1979. This Authority was given pursuant to the National Dam Inspection Act, Public Law 92-367 and by agreement between the State and the U.S. Army Engineers District, Philadelphia. The inspection discussed herein was performed by Anderson-Nichols & Company, Inc.

b. Purpose: The purpose of the Phase I Investigation is to develop an assessment of the general conditions with respect to the safety of Hope Lake Dam and appurtenances. Conclusions are based upon available data and visual inspection. The results of this study are used to determine any need for emergency measures and conclude if additional studies, investigations, and analyses are necessary and warranted.

1.2 Project Description

a. Description of Dam and Appurtenances. Hope Lake Dam is a 233-foot long 8.6-foot high earthfill, stone masonry, and concrete structure. The dam crest is approximately 12.5 feet wide with 2.5H:1V slope brush covered earthen embankment on the upstream side. The downstream embankment at Hope Lake Dam is tree covered with a 2H:1V slope. The dam crest is grass covered with small trees growing on it as well. The concrete capped, stone masonry principal spillway is located on the right side of the dam and is 60 feet long and 2 feet wide. A stoplog section is located approximately in the middle of the dam and consists of four 4"x 8" planks placed in a 4'x 4' bay. The concrete capped, stone masonry emergency spillway is located near the left abutment and is 52.4 feet long with a crest width of about 8 inches, it has a concrete slab apron upstream and a 6.5 foot downstream apron. At the end of the left abutment there is a small canal that is about 9 feet wide at the inlet, that formerly used to supply water power for a mill about a quarter mile downstream.

b. Location. Hope Lake Dam is located on Beaver Brook in Hope Township, Warren County, New Jersey. The Dam is at 40° 54.5' north latitude 74° 58.0' west longitude on the Blairstown Quadrangle. A location map has been included as Figure 2. The dam can be reached by taking exit 12 off Rt. 80 west, onto Rt. 521 south. The dam is on the left a mile from the Rt. 521 exit.

c. Size Classification. Hope Lake Dam is classified as being small in size on the basis of storage at the top of dam of 100 acre-feet, which is less than 1000 acre-feet but more than 50 acre-feet, and on the basis of its structural height of 8.8 feet, which is less than 40 feet, in accordance with criteria given in the Recommended Guidelines for Safety Inspection of Dams.

d. Hazard Classification. Visual inspection of the area below Hope Lake Dam indicated that a single house of about 0.1 mile downstream on the left bank could have up to 6 feet of flood water in the garage beneath the house from either overtopping or breaching of the dam. About two feet of overtopping of the road crossings downstream of the house, would likely result in considerable property damage and possible loss of life. For these reasons, the dam is given a significant hazard classification.

e. Ownership. The dam is owned by Mr. & Mrs. Charles Southwick, P.O. Box 282, Milbrook Road, Hope, New Jersey; for information they may be reached at the above address.

f. Purpose. The original purpose of Hope Lake Dam was to generate power for the downstream mill; recreation is its present purpose.

g. Design and Construction History. No information regarding the original plan or design of the dam was available. Mrs. Southwick said that the dam was originally built by Moravians about 1769. The mill race was dug out by hand using adzes.

h. Normal Operational Procedure. No operational procedures exist for the dam.

i. Site Geology. No site specific geologic information (such as borings) was available at the time the dam was inspected. Information derived from the Geologic Map of New Jersey (Lewis and Kummel, 1912) and Glacial Drift Map of New Jersey (Kummel and Peet, 1902) indicates that the soils within the immediate site area consist of stratified glacial deposits in the form of sands and gravels, deltas, eskers, kames, and terraces.

The depth to bedrock at the dam site is unknown. From the reports previously mentioned, bedrock in this area consists of massive to thin bedded limestones which are Cambrian to Ordovician in age. However, bedrock exposure in the 16-foot cut for the mill race is a dark, fissile, steeply dipping shale. This exposure is about 200 feet downstream of the dam.

### 1.3 Pertinent Data

#### a. Drainage Area

7.7 square miles

#### b. Discharge at Damsite (cfs)

Maximum flood at damsite - unknown.

Total ungated spillway capacity at maximum elevation - 337 (with stoplogs in place)

#### c. Elevation (ft. above NGVD)

Top of dam - 426.0

Maximum pool design surcharge (1/2 PMF) - 430.3

Recreation pool (at time of inspection) - 424.9

Spillway crest - 424.7

Streambed at centerline of principal spillway - 420.4

Maximum tailwater (estimated) - 422.8  
(10 ft downstream of dam)

#### d. Reservoir (feet)

Length of maximum pool - 2600 (estimated)

Spillway crest - 1800

#### e. Storage (acre-feet)

Spillway crest - 64

Design surcharge (1/2 PMF) - 725

Top of dam - 100

#### f. Reservoir Surface (acres)

Top of dam - 25 (estimated)

Spillway crest - 12.8

g. Dam

Type - earthfill, stone masonry, and concrete

Length - 233 feet

Height - 8.6 feet (hydraulic)

- 8.8 feet (structural)

Top width - 12.5 feet

Side slopes - upstream 2.5 H:1V, downstream 2H:1V

Zoning - unknown

Impervious core - unknown

Cutoff - unknown

Grout curtain - unknown

h. Principal Spillway

Type - Concrete capped stone masonry

Length of weir - 60

Crest elevation - 424.7 feet NGVD

Low level outlet - none

U/S channel - Hope Lake

D/S channel - Beaver Brook

i. Emergency Spillway

Type - Concrete capping over stone masonry

Length of weir - 52.4

Crest elevation - 425.2

Gates - none

U/S channel - Hope Lake

D/S channel - Beaver Brook

j. Stoplog Spillway

Type - 4"x8" wood planks (4.5 ft long)

Length of weir - 4 feet

Crest elevation - 425.6 (with stoplogs) 421.6 (without stoplogs)

U/S channel - Hope Lake

D/S channel - Beaver Brook

SECTION 2  
ENGINEERING DATA

2.1 Design

No original plans, hydraulic or hydrologic data for Hope Lake Dam were available.

2.2 Construction

No data concerning the original construction of Hope Lake Dam were revealed; however, owner indicated that it was built over 200 years ago.

2.3 Operation

No data pertaining to the operation of the dam were found.

2.4 Evaluation

- a. Availability. A search of the New Jersey Department of Environmental Protection Files and contact with representatives of the owner of the dam revealed no pertinent information.
- b. Adequacy. Evaluation was based primarily on visual observations and measurements which were adequate for this study.

SECTION 3  
VISUAL INSPECTION

**3.1 Findings**

a. Dam. The area at the downstream toe of the dam is generally wet and soft and some clear seepage water is discharging. Trees are growing on the upstream slope, crest, on the downstream slope and in the area at the downstream toe of the dam. A large tree has been uprooted from the crest near the spillway at the right abutment and its root ball has been pulled out, leaving a large hole on the crest. Roots of trees were observed extending from the upstream slope near the water line toward the downstream edge of the crest.

The crest of the dam is partially covered with grass with a pedestrian path extending along the entire length. Considerable erosion has taken place on the upstream slope at and above the water line. The downstream slope has undergone considerable erosion and slumping adjacent to each of three spillways. In addition, erosion has occurred along portions of the toe that is due to water passing over the spillways and flowing adjacent to the toe in the discharge channels.

b. Appurtenant Structures.

(1) Ungated emergency spillway - left end. The concrete weir is badly eroded and irregular, and the downstream dry stone masonry wall has collapsed in several areas undermining the concrete apron. The entrance to the spillway is partially clogged with wood and grass vegetation. The left training wall is cracked and has settled approximately 1.5 inches.

(2) Gated spillway - middle of dam. The concrete walls and sill of the stoplog facility are badly eroded and spalled. Considerable undermining has occurred around the abutments of the spillway walls. An attempt to reduce erosion and seepage using gunite, sand bags, concrete, concrete blocks, and bags of cement beneath and adjacent to the spillway has not been successful. The wood stoplog gate is deteriorated and is leaking around the ends and through the joints. The wooden bridge is also badly weathered. The concrete block, cast-in-place concrete and stone masonry walls on top of the dam extending right and left from the gated spillway are cracked, irregular, and show considerable leakage on both sides. The downstream face is badly eroded and undermined on both sides of the spillway.

(3) Ungated principal spillway - right end. The crest of the spillway is cracked and eroded, and the downstream face is badly spalled causing undermining of the spillway. Seepage was noted near the left end of the spillway where the original crest had been repaired for about 5 feet from the left abutment of the spillway with stones and concrete.

c. Reservoir Area. The watershed above the lake is gently sloping and wooded. Some open fields exist along the west side of the reservoir. Slopes on the shore of the lake appear to be stable. Evidence of significant sedimentation was observed.

d. Downstream Channel. Considerable erosion has occurred on the right and left bank of each channel immediately downstream of the spillways for a distance of approximately 100 to 150 feet. Trees are growing on the banks of the channels and within the confines of the channels.

SECTION 4  
OPERATIONAL PROCEDURES

**4.1 Procedures**

No formal operating procedures were revealed.

**4.2 Maintenance of Dam**

No formal maintenance procedures for the dam were found.

**4.3 Maintenance of Operating Facilities**

No formal maintenance procedures for the operating facilities were discovered.

**4.4 Warning System**

No description of any warning system was found.

**4.5 Evaluation of Operational Adequacy**

Because of the lack of operation and maintenance procedures, the remedial measures described in Section 7.2 should be implemented as described.

## SECTION 5 HYDROLOGIC/HYDRAULIC

### 5.1 Evaluation of Features

- a. Design Data. Because no data were revealed an evaluation of the hydrologic/hydraulic data could not be performed.
- b. Experience Data. No experience data were found.
- c. Visual Observation. Erosion at left abutment of the principal spillway has been patched with stones (6"-8") and mortar. This area shows some leakage. The crest of the emergency spillway shows considerable spalling. The stone masonry beneath the emergency spillway slab apron has fallen along the downstream face leaving much of the slab without support. Water is leaking through the stone masonry (estimate about 5 to 10 gpm). The stoplog spillway training walls are structurally in poor condition. The stoplog notches are eroded with leakage around the ends and between the logs. The dam has no other low level outlet.
- d. Hope Lake Overtopping Potential. The hydraulic/hydrologic evaluation for the dam is based on a selected Spillway Design Flood (SDF) equal to one-half the Probable Maximum Flood (PMF) in accordance with the range of test floods given in the evaluation guidelines, for dams classified as significant hazard and small in size. The PMF was determined by application of a 24-hour probable maximum storm of 23.1 inches to the SCS dimensionless unit hydrograph. Hydrologic computations are given in Appendix 3. The routed one-half PMF peak discharge for the subject drainage area is 8,385 cfs.

The minimum elevation of the dam allows 1.3 foot of depth above the principal spillway, 0.8 foot above the emergency spillway and 0.4 foot above the stoplog spillway (with stoplogs in place) before overtopping occurs. Under this head the total spillway capacity for the 3 spillways is 337 cfs, which is less than the selected SDF (approximately 4 percent).

At discharges above 6900 cfs, the backwater resulting from the narrowing and gradual slope of the channel downstream of the dam begins to cause slightly less flow over the dam than would occur without this backwater effect. Because this effect was found to be negligible for Hope Lake Dam, the discharge coefficient for the spillway weir was not changed. Calculations are shown in Appendix 3.

Flood routing calculations indicate that Hope Lake Dam will be overtopped for 13.2 hours to a maximum depth of 4.3 feet under one-half PMF conditions. It is estimated that the principal spillway can pass 2 percent (240 cfs) of the one-half PMF without overtopping the dam; thus, the spillway is considered inadequate.

3. Drawdown Capacity. There are no drawdown pipes for Hope Lake Dam.

## SECTION 6 STRUCTURAL STABILITY

### 6.1 Evaluation of Structural Stability

a. The soft, wet areas and seepage at the downstream toe of the dam is indicative of seepage through and under the dam, which, if not properly controlled, could lead to failure of the dam by piping or sloughing of the downstream slope. Trees growing on the crest and on the upstream and downstream slopes may cause seepage and erosion problems if a tree blows over and pulls out its roots, or if a tree dies or is cut and its roots rot. One large tree has already blown over, leaving a hole in the crest where its roots pulled out and this hole weakens the crest. Erosion at the abutments of the spillways and seepage below and adjacent to these structures could lead to breaching of the dam at these locations if not controlled. Erosion caused by overtopping of the upstream concrete walls on either side of the center spillway could lead to breaching.

Erosion of the upstream slope at the water line could eventually lead to breaching of the dam.

**6.2 Design and Construction Data.** No design or construction data pertinent to the structural stability of the dam are available.

**6.3 Operating Records.** No operating records pertinent to the structural stability of the dam were available.

### 6.4 Post-Construction Changes

No record of post-construction changes was available. However, evidence of numerous patchings are clearly visible.

**6.5 Seismic Stability** - This dam is in Seismic Zone 1. According to the Recommended Guidelines, dams located in Seismic Zone 1 "may be assumed to present no hazard from earthquake provided static stability conditions are satisfactory and conventional safety margins exist." None of the visual observations made during the inspection are indicative of unstable slopes. However, because no data are available concerning the engineering properties of the embankment and foundation materials for this dam, it is not possible to make an engineering evaluation of the stability of the slopes or the factor of safety under static conditions.

SECTION 7  
ASSESSMENT, RECOMMENDATIONS/REMEDIAL MEASURES

**7.1 Dam Assessment**

- a. Condition. Hope Lake is probably over 200 years old and is in very poor condition.
- b. Adequacy of Information. The information available is such that the assessment of the dam must be based entirely on the results of the visual inspection.
- c. Urgency. The recommendations made in 7.2.a and 7.2.b should be implemented by the owner as prescribed.
- d. Necessity for Additional Data/Evaluation. The information available from the visual inspection is adequate to identify the potential problems which are listed in 7.2.a. These problems require the attention of a professional engineer who will have to make additional engineering studies to design or specify remedial measures to rectify the problems. If left unattended, the problems could lead to failure of the dam.

**7.2 Recommendation/Remedial Measures**

**a. Recommendations**

The owner should retain a professional engineer qualified in the design and construction of dams to accomplish the following in the time periods specified:

**Immediately:**

Investigate the cause of the seepage and wet, soft areas at the downstream toe of the dam.

**Very soon:**

- (1) Design procedures for and inspect the removal of the trees and their roots from the entire embankment.
- (2) Design procedures for and inspect the construction of erosion protection on the upstream slope of the dam.
- (3) Design procedures for the repair or replacement of the gated and ungated spillways where considerable erosion and seepage are taking place.

- (4) Design channels to reroute the flowing water away from the toe of the dam.
- (5) Establish procedures and supervise backfilling of the embankment sections on either side of the stoplog spillway.

In the near future:

- (1) Further evaluate the hydrology and hydraulics of the watershed, reservoir, dam, and spillways, and design and implement necessary mitigating measures. Items b(2) and b(3) following should be considered in conjunction with this recommendation.
- (2) Design and install adequate means to drain the reservoir in case of emergency.

b. Operating and Maintenance Procedures

The owner should do the following immediately:

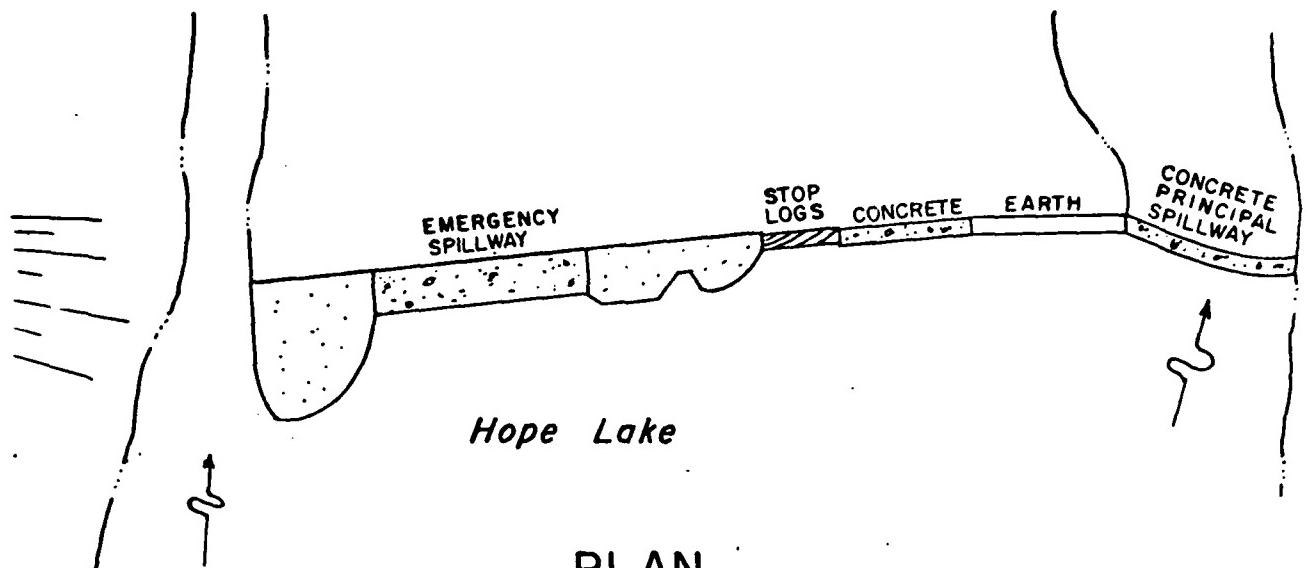
- (1) Clear debris and trees from the spillway discharge channels and maintain the channels free from debris.
- (2) Check the condition of the dam periodically.
- (3) Clear brush and uncontrolled vegetation from slopes of the dam and keep the slopes free from all debris.
- (4) Clear trees and brush for some distance downstream from the toe of the dam and from the banks of the discharge channels for some distance downstream from the spillways.

In the near future:

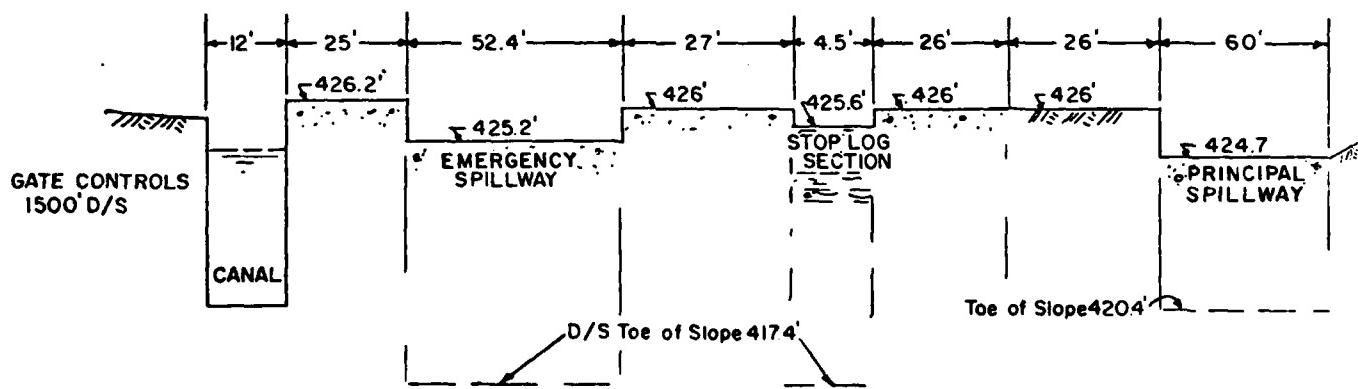
Develop written operation procedures and a periodic maintenance plan to ensure the safety of the dam.

In the future:

Establish a surveillance program for use during and immediately following periods of heavy rainfall and also a warning program to follow in case of emergency conditions.



## PLAN



## ELEVATION

Anderson-Nichols & Co, Inc BOSTON MASSACHUSETTS		U.S. ARMY ENGINEER DIST PHILADELPHIA CORPS OF ENGINEERS PHILADELPHIA, PA	
NATIONAL PROGRAM OF INSPECTION OF NON-FED.DAMS			
HOPE LAKE DAM			
BEAVER BROOK		NEW JERSEY	
		SCALE NOT TO SCALE	
		DATE MAY 1981	FIGURE 1



Anderson-Nichols & Co., Inc.

BOSTON

MASSACHUSETTS

U.S. ARMY ENGINEER DIST. PHILADELPHIA CORPS OF ENGINEERS  
PHILADELPHIA, PA.

NATIONAL PROGRAM OF INSPECTION OF NON-FED.DAMS

'HOPE LAKE DAM  
LOCATION MAP

BEAVER BROOK

NEW JERSEY

MAP BASED ON STATE OF NEW JERSEY  
OFFICIAL MAP & GUIDE.

SCALE IN MILES



SCALE: 1" = 4 Miles Approx.

DATE: MAY 1961

FIGURE 2

**APPENDIX 1**

**CHECK LIST**

**VISUAL INSPECTION**

**HOPE LAKE DAM**

Check List  
Visual Inspection  
Phase 1

Name Dam	Hope Lake (NJ00796)	County	Warren	State	New Jersey	Coordinators	NJDEP
Date(s) Inspection	2/16/81		Fair, clear				36°
	4/22/81	Weather	Clear, cold		Temperature		38°
Pool Elevation at Time of Inspection	424.9	NGVD	Tailwater at Time of Inspection	418.2	NGVD		

Inspection Personnel:

W. Guinan	S. Gilman
J. Stone	R. Murdock

Guinan/Gilman Recorder

Mrs. Charles Southwick, owner, was present with the inspection party.

**UNGATED SPILLWAY**  
Right End of Dam

**VISUAL EXAMINATION OF**

**OBSERVATIONS**      **REMARKS OR RECOMMENDATIONS**

**CONCRETE WEIR**

Concrete weir is curved. Top surface is eroded and cracked. Right ends show evidence of movement. Downstream face is badly eroded and spalled undermining face and bottom of wall. Left end has been repaired with mortared cobbles - 6-8 in +. Seepage and leakage noted at both ends of spillway.

Major reconstruction required.

**APPROACH CHANNEL**

Under water, appears to be shallow, unobstructed.

**DISCHARGE CHANNEL**

Debris, fallen trees, boulders in bottom channel, joins with discharge channel for gated spillway.

Clear trees and brush 25 ft on either side of discharge channel for a distance of 100 ft downstream from the dam or to the property line, whichever is less.

**BRIDGE AND PIERS  
OVER SPILLWAY**

None

Stop Log Section and Adjacent Concrete Dam

GATED SPILLWAY  
at Center of Dam

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SILL	Bottom of stop log section is eroded & deteriorated in +.	Major construction required of entire structure.
APPROACH CHANNEL	Upstream face of stop log section is badly deteriorated with concrete cap showing evidence of forward movement.	
DISCHARGE CHANNEL	Sidewalls are badly cracked and spalled. Some repairs have been made with mortared stone.	Clear trees and brush 25 ft on either side of discharge channel for a distance of 100 ft downstream from the dam.
BRIDGE AND PIERS	2 in wood planks are badly weathered with some deterioration.	See note above Major Construction
GATES AND OPERATION EQUIPMENT	Stop logs are deflected. All planks show evidence of deterioration. Leakage is observed around ends of stop log and thru joints. Stop log slots are badly eroded.	See note above Major Construction
CONCRETE DAM WALLS ADJACENT TO GATED SPILLWAY	Walls are cracked, irregular and show considerable leakage on both sides. D/S face is badly eroded and undermined on both sides.	See note above Major Construction

**UNGATED SPILLWAY**  
**Left End of Dam**

**VISUAL EXAMINATION OF**

**OBSERVATIONS**      **REMARKS OR RECOMMENDATIONS**

**CONCRETE WEIR**  
The top of the concrete weir is badly eroded and uneven. D/S apron is in fair condition. Left training wall is cracked and has settled 1.5 in. Dry stone masonry wall on d/s face has collapsed in several areas.

Repair concrete weir. Repair dry stone masonry wall.

**APPROACH CHANNEL**

Under water, appears to be shallow, unobstructed.

**DISCHARGE CHANNEL**

Debris, fallen trees, boulders in bottom channel, joins with discharge channel for gated spillway. Clear trees and brush 25 ft on either side of discharge channel for a distance of 100 ft downstream from the dam or up to the property line, whichever is less.

**BRIDGE AND PIERS  
OVER SPILLWAY**

None.

## EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None observed.	
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None apparent.	
SLoughing or Erosion of embankment and abutment slopes	Pronounced erosion on both upstream and downstream slopes. Trees present on both slopes.	Control trespassing on dam. Repair erosion on dam.
Vertical and horizontal alignment of the crest	Horizontal alignment - fair. Vertical alignment - right undulation of crest.	
RIPRAP FAILURES	Slight amount of riprap evident below water surface. Only a few riprap pieces present on the slope.	

## EMBANKMENT

## VISUAL EXAMINATION OF

## OBSERVATIONS      REMARKS OR RECOMMENDATIONS

## RAILINGS

None apparent.

JUNCTION OF EMBANKMENT  
AND ABUTMENT, SPILLWAY  
AND DAM

Erosion at both abutments and at junction with spillway structure.  
See Notes in "Ungated Spillway"  
regarding concrete walls along embankment.

## ANY NOTICEABLE SEEPAGE

Seepage evident below and adjacent to spillway, emergency spillway and gated spillway.

Investigate seepage and design appropriate remedial measures.

## STAFF GAGE AND RECORDER

None apparent.

## DRAINS

None apparent.

INSTRUMENTATION			
VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS	
MONUMENTATION/SURVEYS	None apparent.		
OBSERVATION WELLS	None apparent.		
WEIRS	None apparent.		
PIEZOMETERS	None apparent.		
OTHER	None apparent.		

RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SLOPES	Gradual slopes, wooded. Open fields.	
SEDIMENTATION	Appears to be significant sedimentation in the reservoir.	

DOWNSTREAM CHANNEL

VISUAL EXAMINATION OF CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
Debris, boulders in channel: Banks heavily overgrown with trees and vines.		
SLOPES	Trees and brush covered, gentle slopes on the right bank; tree- and brush-covered steep slopes with a flat flood plain on the left bank.	One house about 0.1 mile downstream on left bank with 2 residents. The first floor is about 14 feet above the channel invert. Three empty buildings (corn canning plant) on the right bank are within 100 yards of the dam with a first floor elevation from 8 to 10 ft above channel bottom.

APPROXIMATE NO.  
OF HOMES AND  
POPULATION

CHECK LIST  
ENGINEERING DATA  
DESIGN, CONSTRUCTION, OPERATION

ITEM	REMARKS
PLAN OF DAM	None found
REGIONAL VICINITY MAP	Prepared for this report
CONSTRUCTION HISTORY	None found
TYPICAL SECTIONS OF DAM	None
HYDROLOGIC/HYDRAULIC DATA	None
OUTLETS - PLAN	None found
- DETAILS	None found
- CONSTRAINTS	None found
- DISCHARGE RATINGS	None found
RAINFALL/RESERVOIR RECORDS	None found

ITEM		REMARKS
DESIGN REPORTS	None found	
GEOLOGY REPORTS	None found	
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	None found	
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	None found	
POST-CONSTRUCTION SURVEYS OF DAM	None found	
BORROW SOURCES	Unknown	

ITEM	REMARKS
MONITORING SYSTEMS	None
MODIFICATIONS	None
HIGH POOL RECORDS	None
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None
MAINTENANCE OPERATION RECORDS	None

ITEMS	REMARKS
SPIIWAY PLAN	Prepared for this report from field inspection
SECTIONS	None
DETAILS	None
OPERATING EQUIPMENT PLANS & DETAILS	None

CHECK LIST  
HYDROLOGIC AND HYDRAULIC DATA  
ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: 7.7 square miles, gentle slope,  
woods.

ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 424.7' NGVD  
(64 acre-feet).

ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY)  
Not applicable

ELEVATION MAXIMUM HIGH POINT ON DAM: 426.2' NGVD

ELEVATION TOP DAM: 426.0' NGVD

PRINCIPAL SPILLWAY CREST: Uncontrolled concrete capped stone  
masonry

a. Elevation 424.7' NGVD

b. Type Concrete

c. Width 2 feet

d. Length 60 feet

e. Location Spillover Right end of dam

f. Number and Type of Gates None

EMERGENCY SPILLWAY CREST: Free overflow concrete spillway

a. Elevation 425.2' NGVD

b. Type Concrete

c. Width 12.5 feet w/aprons up and downstream

d. Length 52.4 feet

e. Location Spillover Left of center of dam

f. Number and Type of Gates None

STOPLOG SECTION: 4" x 8" wood planks

- a. Elevation 426.5" NGVD
- b. Type Wood planks
- c. Width 4 inches
- d. Length 4.5 feet
- e. Location Spillover Center of dam
- f. Number and Type of Gates Four 4" x 8" stoplogs

OUTLET WORKS: None

HYDROMETEOROLOGICAL GAGES: None

MAXIMUM NON-DAMAGING DISCHARGE: 337 cfs (Total spillway capacity)

**APPENDIX 2**

**PHOTOGRAPHS**

**HOPE LAKE DAM**



21 April 1981

Spillway crest looking toward left (east) side of dam



21 April 1981

Looking eastward across emergency spillway crest and apron



21 April 1981

View of downstream face of emergency spillway



21 April 1981

Looking u/s at stoplog spillway



21 April 1981

View of undermining of concrete cap on stoplog  
spillway training wall.



21 April 1981

Outside and d/s appearance of right training wall of  
stoplog spillway



18 February 1981

Looking u/s across Hope Lake Reservoir



21 April 1981

Spillway channel looking downstream

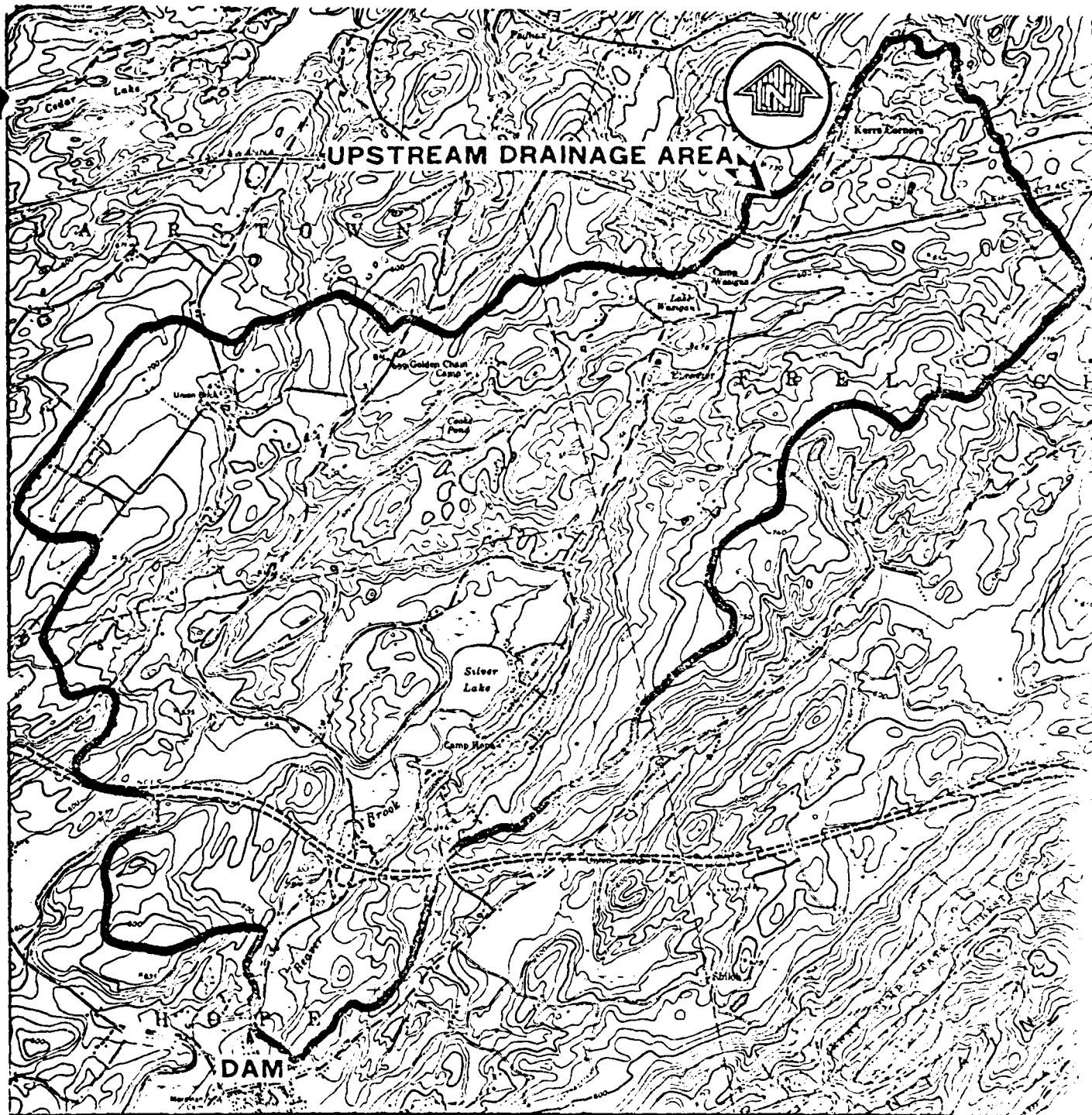


21 April 1981

Mill Race looking d/s near left (east) end of dam

APPENDIX 3  
HYDROLOGIC COMPUTATIONS

HOPE LAKE DAM



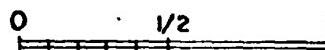
NATIONAL PROGRAM OF INSPECTION OF  
NON-FED. DAMS

HOPE LAKE DAM  
HOPE TOWNSHIP, NEW JERSEY

REGIONAL VICINITY MAP  
MAY 1981

DEPARTMENT OF THE ARMY  
PHILADELPHIA DISTRICT, CORPS OF ENGINEERS  
PHILADELPHIA, PENNSYLVANIA

SCALE IN MILES



MAP BASED ON U.S.G.S. 7.5 MINUTE QUADRANGLE  
SHEET. BLAIRSTOWN, N.J. 1954, REVISED 1971.

JOB NO.

Sheet No. 1 of 1  
Date 5/15/81  
Computed C.H.P.  
Checked R.E.S.SQUARES  
1/4 IN. SCALE

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29

1 TIME OF CONCENTRATION  
23 ① Texas Highway Method.  
4

5 overland

6 woodlands

7 reach = 5000'

8  
9 slope =  $\frac{734 - 600}{5000} = 0.027$   
10

11 ave vel = 1 fps  $\frac{2000 \text{ ft}}{1 \text{ ft/sec}} = 6000 \text{ sec}$   
12  
13  
14 = 83 min = 1.4 hrs.  
15

16 channel

17 reach = 25,000'

18 slope =  $\frac{600 - 435}{25,000} = .007$   
19

20 ave vel = 2 fps  $\frac{25000'}{1 \text{ sec}} = 12500 \text{ sec}$   
21  
22  
23  
24  
25 = 208 min = 3.5 hrs  
26

27 TOTAL  $t_c = 1.4 + 3.5 = 4.9$  hrs  
28

29  
30 ② Soil & Water Conservation

31  $L = \frac{s^{0.8} (s+1)^{1.67}}{9000 y^{0.5}}$   $\text{CN} - 10$   
32  
33  
34

35  $L = 5000 + 25000 = 30,000'$   
36

37  $CN = 70 \text{ for } L = 30,000'$   
38

$s = \frac{1000}{70} - 10 = 6.1$

39  $y = \frac{.027 + .007}{2} = 0.017 = 1.7\%$

JOB NO.

SQUARES  
1/4 IN. SCALE 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

$$L = \frac{(30,000)^{0.8} (4.3+1)^{1.67}}{9000 (17)^{0.5}} = 5.2 \text{ hrs}$$

$$T_c = \frac{L}{.6} = \frac{5.2}{.6} = 8.7 \text{ hrs}$$

### (3) SCS TR #55 method

overland

$$l = 5,000 \text{ head} = 134'$$

$$\text{slope} = 0.027 \quad \text{woodland}$$

from plot of % slope vs. velocity,  $V = 4 \text{ fps}$

$$\frac{5000 \text{ ft}}{4 \text{ ft/sec}} = 1250 \text{ sec} = 0.35 \text{ hrs}$$

channel

$$l = 25,000' \quad \text{slope} = 0.007 \quad n = .03$$

$$V = \frac{1.49}{n} R^{2/3} S^{1/2}$$

(assume 1' x 10' rectangular channel /  
to calculate  $R$ )

$$R = \frac{A}{wP} = \frac{10}{2(10) + 10} = 0.83 \text{ ft}^2$$

$$V = \frac{1.49}{.03} (0.83)^{2/3} (.007)^{1/2} = 3.7 \text{ ft/sec}$$

$$\frac{25000 \text{ ft}}{3.7 \text{ ft/sec}} = 6793 \text{ sec} = 1.9 \text{ hrs}$$

$$\text{TOTAL} = 1.9 + 3.5 = \underline{\underline{5.4 \text{ hrs}}}$$

JOB NO.

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29

1/4 IN. SCALE

## (4) Kerby Method

$$T_c = 0.83 \left( \frac{Nl}{\sqrt{s}} \right)^{0.467}$$

$$l = 5000' \quad s = .027 \quad N = 0.60$$

$$T_c = 0.83 \left[ \frac{(0.6)(5000)}{\sqrt{.027}} \right]^{0.467} = \underline{1.4 \text{ hrs}}$$

for channel use

Manning's, as Method 3

$$V = 3.6 \text{ f/s} \quad \frac{25 \text{ CFS ft}}{3.6 \text{ ft/sec}} = 6944 \text{ sec} = \underline{1.9 \text{ hrs.}}$$

$$T_c = 1.4 + 1.9 = \underline{3.3 \text{ hrs.}}$$

$$\text{ave } T_c = \frac{4.9 + 8.7 + 5.4 + 3.3}{4} = 5.6 \text{ hrs}$$

$$T_{lag} = 0.6 \times 5.6 = \underline{3.3 \text{ hrs}}$$

X

JOB NO.

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

1

2

## STAGE - STORAGE DETERMINATIONS

3

4

ASSUME DEPTH OF LAKE TO BE 5 FEET

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6

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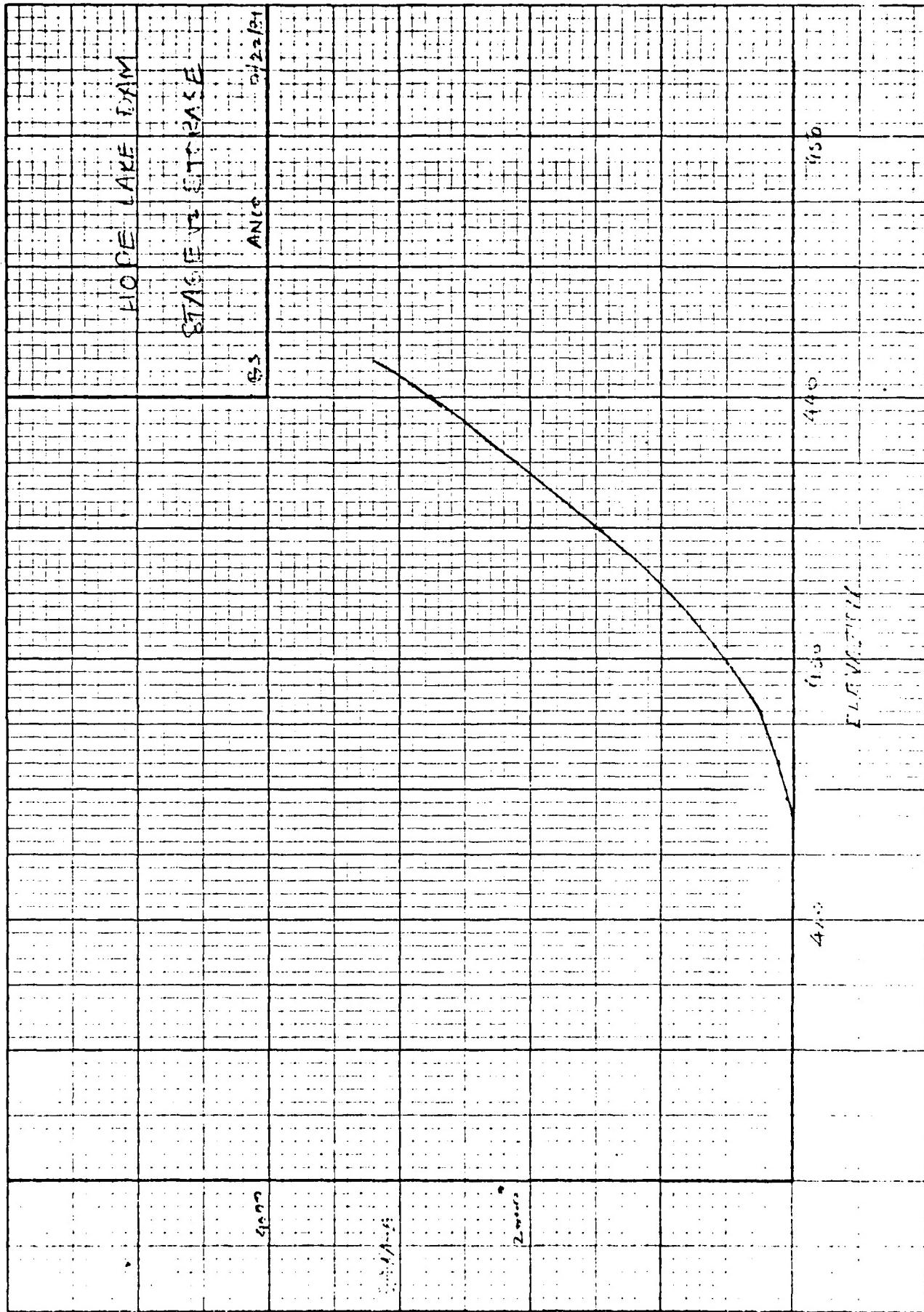
38

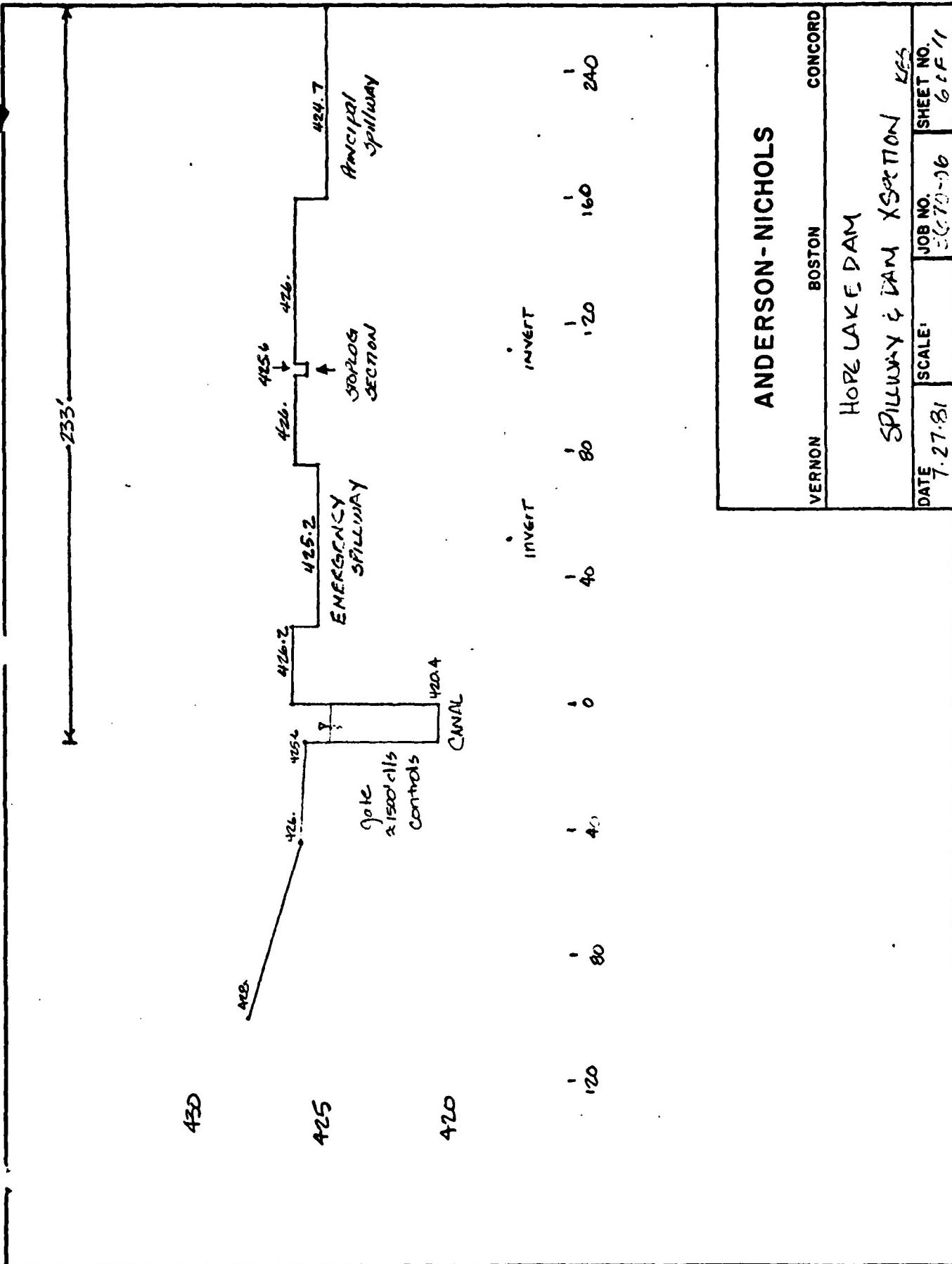
39

Elevation	SURFACE AREA ACRES	AVG SA. ACRES	INCREMENTAL Storage AC-Ft	CONTINUATIVE Storage AC-Ft
424.7	12.8	12.8	64	64
440	345.6	176	2692.8	2756.8
460	614.4	480	9600	12356.8

Input for HEC-I (from curve)

Stage	Storage
424.0	0
424.7	64
430.0	70
435.0	85
440.0	110
426.2	115
428.0	120
430	520
432.0	850
435.0	1500
440.0	2757





ANDERSON-NICHOLS

VERNON            BOSTON            CONCORD

HOPE LAKE DAM

SPILLWAY & DAM SECTION

DATE: 7.27.81    SCALE: 1:16    JOB NO. E-70-16    SHEET NO. 6 of 11

## **Anderson-Nichols & Company, Inc.**

Subject Hope Lakin

Sheet No. 7 of 11  
Date 5/11/11  
Computed C.L.  
Checked K.E.S.

JOB NO.

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30  
1/4 SCALE

## DEVELOPMENT OF RATIOS CIRCLE

$$Q = C l \cdot H^{3/2}$$

## ① Spillway Closure

$c = 2.7$     $L = 60$    width = 2.0

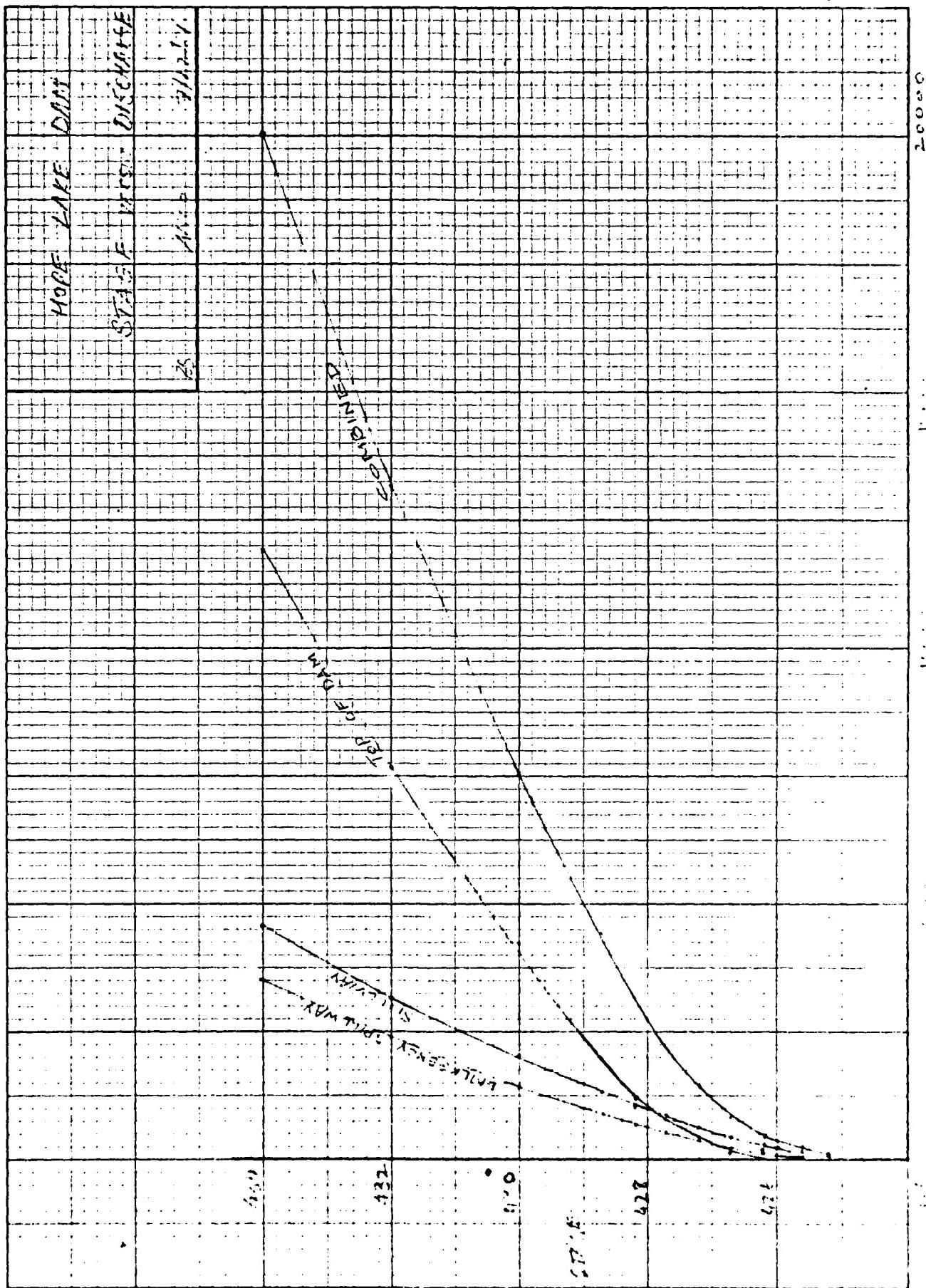
② Top of dam curve

$$c = a \cdot b \quad L = 153^{\circ} \quad \text{width} = 12.5$$

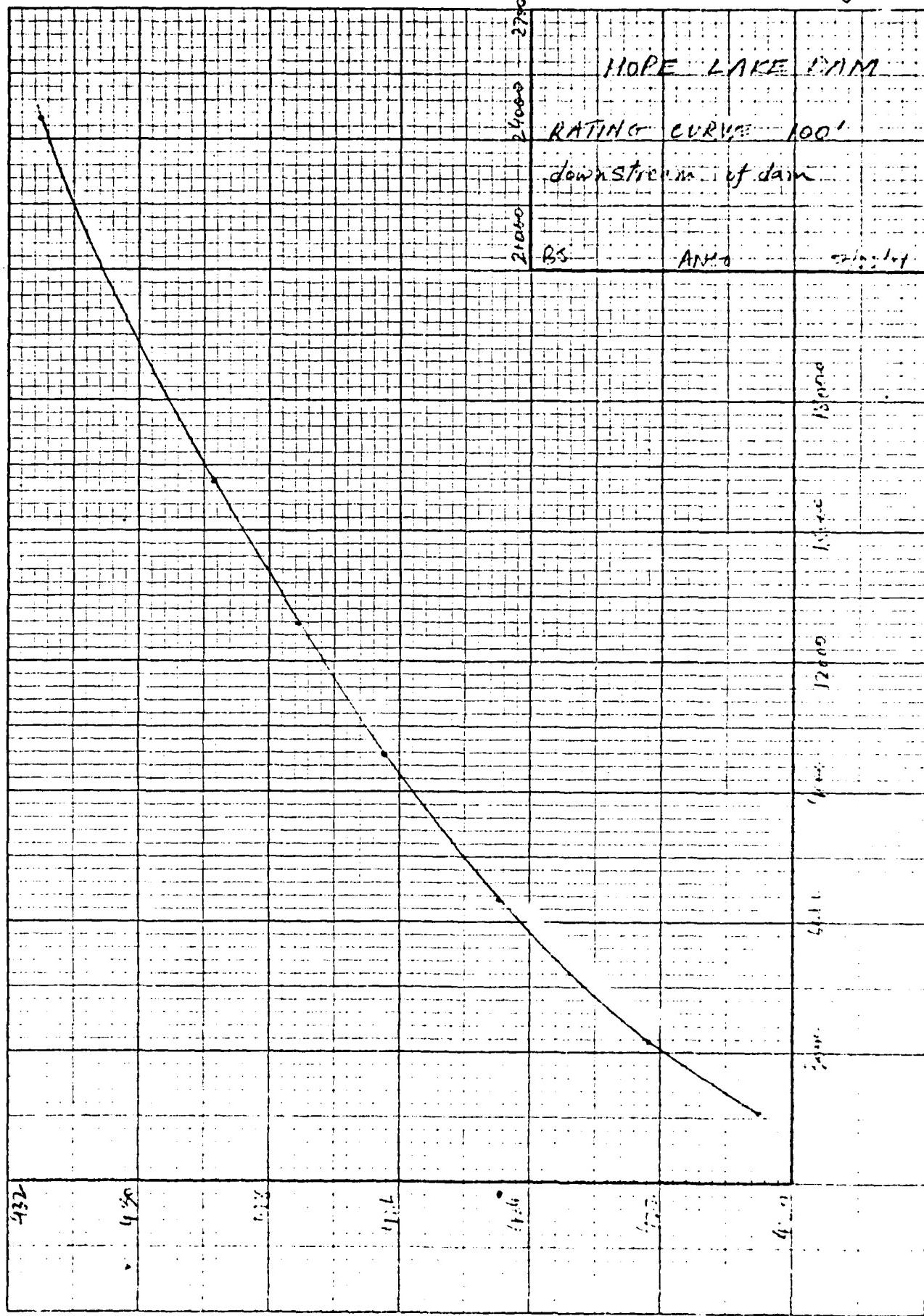
### ③ Emergency Spillway

$$c=2.6 \quad L=52 \quad \text{width} = 6.5$$

	Elevation	Principal spillway	Emergency spilling	TOP of D.A.W.			Comb. Q.		
		head	Q	head	Q	head	length	Q	
14	424.7	0							
15	425.2	0.5	57.2	0					57
16	"25.6	1.0	162	0.5	18				210
17	426.0	1.3	240	0.8	97				337
18	426.2	1.5	298	1.0	135				433
19	426.7	2.0	458	1.5	248	0.5	153	140	246
20	427.2	2.5	540	2.0	332	1.0	170	442	442
21	427.7	3.0	842	2.5	534	1.5	170	312	2193
22	428.2	3.5	1061	3.0	701	2.0	190	517	517
23	428.7	4.0	1276	3.5	934	2.5	190	1153	4133
24	430.0	5.3	1777	4.3	1420	3.8	210	4045	7442
25	432.0	7.3	3195	6.9	2314	5.9	210	7627	13216
26	434.0	9.3	4595	8.3	3524	7.9	210	11314	20203



9 of 11



JOB NO.

## Weir Submergence Calculations

SQUARES  
1/4 IN. SCALE 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

1  
 2 Data for Rating Curve @ 100' downstream  
 3 from HEC-1  
 4  
 5

6 1 FLOW 1646. 3223. 6477. 9782. 12868. 16137. 24513. 33009.  
 7 TIME 19.67 19.83 19.75 19.75 19.83 19.83 19.75 19.67

8 \*\* PEAK STAGES IN FEET \*\*

9 1 STAGE 420.52 422.16 424.45 426.22 427.57 428.82 431.46 433.66.  
 10 TIME 19.67 19.83 19.75 19.75 19.83 19.75 19.67 19.67

11 FROM HEC-1 CALCULATIONS -

12  $\frac{1}{2}$  PMF  $Q = 8114 \text{ CFS}$

13  $\frac{1}{2}$  PMF ELEVATION d/s Xsect. = 425.9'

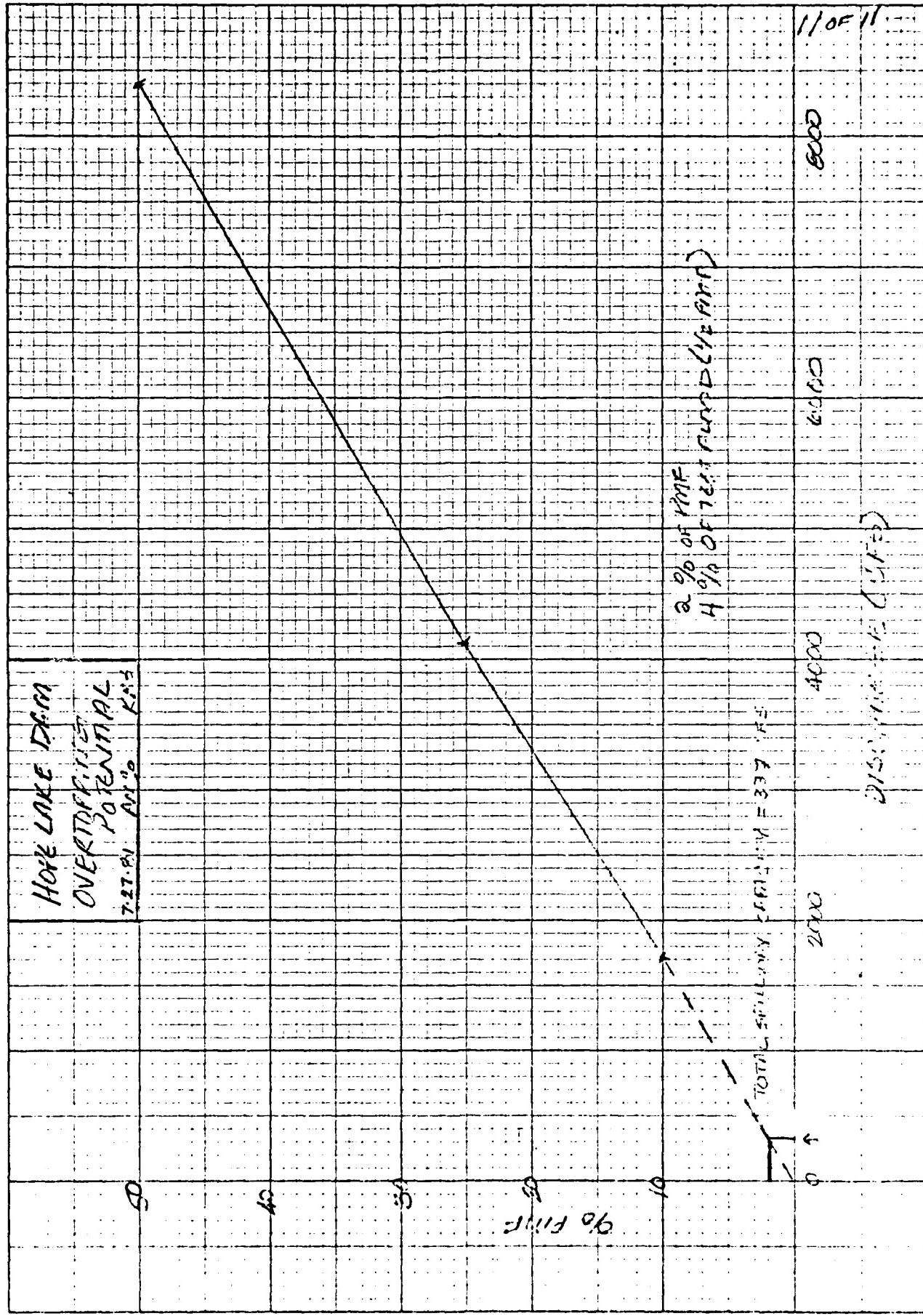
14  $\frac{1}{2}$  PMF ELEVATION dam = 431.2'

15 Calculations of decrease in discharge coefficient  
 16 for submerged orifices (spillway) (using Chow's  
 17 Chow's Open Channel Hydraulics, 1957)



$Q$	Revised Xsect	Revised d	% Change	$hd$	$He$	$d$	$h_f$	$h_t$
8114	425.9	431.2	1.2	5.3	6.5	9.7	0.6	1.2

0.23% reduction in 'C' value for weir (using Chow) - neglect



**APPENDIX 4**  
**HEC-1 OUTPUT**  
**HOPE LAKE DAM**

## HFC-1 INPUT

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
 ID HOPE LAKE DAM ANALYSIS  
 NEW JERSEY DAM NO: 796 HARREN COUNTY  
 0.10 MULTIPLES OF PMF FROM TOWNSHIP OF HOPEVILLE A-NEED INCHES  
 0.25 0.5 0 30C  
 JR FLOW 0.1 0.25 0.5  
 KK ALL HOPE LAKE DAY COMPUTATION  
 KH SLS UNIT GRAPH COMPUTATION  
 64 7.7  
 23.3 23.1 1  
 PH 23.0 .1 5  
 LUU 3.3 NO 111 173 132  
 UD  
 KK A2 ROUTE INFLOW HYDROGRAPH THROUGH HOPE LAKE  
 STOR 64  
 RSV 0 64 70 100 150 210 350 520 650  
 417.4 424.7 425.2 426.7 426.6 427.2 428.7 429.7 430 432  
 417.4 424.7 425.2 426.7 426.7 427.2 428.7 429.7 430. 432.  
 426.0 426.0 426.0 426.0 426.0 426.0 426.0 426.0 426.0 426.0  
 173 173 173 173 173 173 173 173 173 173

FLD07 HYDROGRAPH PACKAGE (HEC-1)  
FLD07 HYDROGRAPH PACKAGE (HEC-1)  
DATE 07/23/81 TIME 17:25:10  
SUB

HUPE LAKE DAM NO. 799 DIVERGING ANALYSIS FOR HOPPERVILLE A-NCCN INC-09  
NEW JERSEY 0.1.0.25.0.5 MULTIPLES OF PMF FROM 24-HOUR PMP

5 10      OUTPUT CONTROL VARIABLES      PRINT CONTROL  
IERNT 2      PLOT CONTROL  
IELUT 0      PLOT GRAPH PLOT SCALE  
USCAL 0      HYDROGRAPH PLOT SCALE  
CMSC YES      PRINT DIAGNOSTIC MESSAGES

17      HYDROGRAPH TIME DATA      5 MINUTES IN COMPUTATION INTERVAL  
NPIN TIME 1 0000 STARTING TIME  
IDATE 1 0000 ENDING TIME  
NO 300 NUMBER OF HYDROGRAPH ORDINATES  
NUDATE 2 005 ENDING TIME  
ADTIME COMPUTATION INTERVAL 0.08 HOURS  
COMPUTATION INTERVAL TIME BASE 24.92 HOURS

ENGLISH UNITS      SQUARE MILES  
DRAINAGE AREA      INCHES  
PRECIPITATION DEPTH      FEET  
LENGTH, ELEVATION      CUBIC FEET PER SECOND  
FLOW      ACRES-FEET  
STORAGE VOLUME      ACRES-FEET  
SURFACE AREA      DEGREES FAHRENHEIT  
TEMPERATURE

JP      MULTI-PLAN OPTION      1 NUMBER OF PLANS  
MLI-RATIO OF RUNOFF 0.10      0.50

7 KK      A1      HOPE LAKE DAM  
SUB BASIN CHARACTERISTICS      70 SUBBASIN AREA  
SCS UNIT GRAPH COMPUTATION

9 BA      SUBBASIN RUNOFF DATA  
SUB BASIN AREA      70 SUBBASIN AREA

5 BF      BASE FLOW CHARACTERISTICS  
SPTO 23.10 INITIAL FLOW  
GRCAN 23.10 BEGIN BASE FLOW RECESSION  
FTRR 1.00000 RECESSION CONSTANT

## PRECIPITATION DATA

PM	PREPARABLE MAXIMUM STORM FHS	INDEX PRECIPITATION TIME POSITION COEFFICIENT
	23.00	0.00
TRSPC	0.00	TRANSPOSITION AREA
TASDA	7.00	NU USE SWD DISTRIBUTION
SWD	NU	
PERCENT OF INDEX PRECIPITATION OCCURRING IN GIVEN TIME		
111.0	12-HR	THE 72-HR
111.0	123.0	0.0
0.0		96-HR
UNIFORM LOSS RATE 1.00 INITIAL LOSS		
LU	STRL	UNIFORM LOSS RATE
CNSTL	0.10	
RTIMP	5.00	PERCENT IMPERVIOUS AREA
SCS DIMENSIONLESS UNITGRAPH		
***		

## UNIT HYDROGRAPH TRUNCATED FROM 200 TO 150 INTERVALS

150 FT-UNIT HYDROGRAPH	
VOLUME	PER 100 ORDINATES
1.00	92.
34.	390.
53.	371.
73.	326.
92.	309.
112.	290.
131.	271.
150.	252.
169.	233.
187.	212.
205.	193.
223.	173.
241.	154.
259.	135.
277.	116.
295.	97.
313.	78.
331.	59.
349.	40.
367.	21.
385.	1.
403.	
421.	
439.	
457.	
475.	
493.	
511.	
529.	
547.	
565.	
583.	
601.	
619.	
637.	
655.	
673.	
691.	
709.	
727.	
745.	
763.	
781.	
799.	
817.	
835.	
853.	
871.	
889.	
907.	
925.	
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**HYDROGRAPH AT STATION A1**

1764 1778 1782 1786 1790 1794 1798 1802 1806 1810 1814 1818 1822 1826 1830 1834 1838 1842 1846 1850 1854 1858 1862 1866 1870 1874 1878 1882 1886 1890 1894 1898 1902 1906 1910 1914 1918 1922 1926 1930 1934 1938 1942 1946 1950 1954 1958 1962 1966 1970 1974 1978 1982 1986 1990 1994 1998 2002 2006 2010 2014 2018 2022 2026 2030 2034 2038 2042 2046 2050 2054 2058 2062 2066 2070 2074 2078 2082 2086 2090 2094 2098 2102 2106 2110 2114 2118 2122 2126 2130 2134 2138 2142 2146 2150 2154 2158 2162 2166 2170 2174 2178 2182 2186 2190 2194 2198 2202 2206 2210 2214 2218 2222 2226 2230 2234 2238 2242 2246 2250 2254 2258 2262 2266 2270 2274 2278 2282 2286 2290 2294 2298 2302 2306 2310 2314 2318 2322 2326 2330 2334 2338 2342 2346 2350 2354 2358 2362 2366 2370 2374 2378 2382 2386 2390 2394 2398 2402 2406 2410 2414 2418 2422 2426 2430 2434 2438 2442 2446 2450 2454 2458 2462 2466 2470 2474 2478 2482 2486 2490 2494 2498 2502 2506 2510 2514 2518 2522 2526 2530 2534 2538 2542 2546 2550 2554 2558 2562 2566 2570 2574 2578 2582 2586 2590 2594 2598 2602 2606 2610 2614 2618 2622 2626 2630 2634 2638 2642 2646 2650 2654 2658 2662 2666 2670 2674 2678 2682 2686 2690 2694 2698 2702 2706 2710 2714 2718 2722 2726 2730 2734 2738 2742 2746 2750 2754 2758 2762 2766 2770 2774 2778 2782 2786 2790 2794 2798 2802 2806 2810 2814 2818 2822 2826 2830 2834 2838 2842 2846 2850 2854 2858 2862 2866 2870 2874 2878 2882 2886 2890 2894 2898 2902 2906 2910 2914 2918 2922 2926 2930 2934 2938 2942 2946 2950 2954 2958 2962 2966 2970 2974 2978 2982 2986 2990 2994 2998 3002 3006 3010 3014 3018 3022 3026 3030 3034 3038 3042 3046 3050 3054 3058 3062 3066 3070 3074 3078 3082 3086 3090 3094 3098 3102 3106 3110 3114 3118 3122 3126 3130 3134 3138 3142 3146 3150 3154 3158 3162 3166 3170 3174 3178 3182 3186 3190 3194 3198 3202 3206 3210 3214 3218 3222 3226 3230 3234 3238 3242 3246 3250 3254 3258 3262 3266 3270 3274 3278 3282 3286 3290 3294 3298 3302 3306 3310 3314 3318 3322 3326 3330 3334 3338 3342 3346 3350 3354 3358 3362 3366 3370 3374 3378 3382 3386 3390 3394 3398 3402 3406 3410 3414 3418 3422 3426 3430 3434 3438 3442 3446 3450 3454 3458 3462 3466 3470 3474 3478 3482 3486 3490 3494 3498 3502 3506 3510 3514 3518 3522 3526 3530 3534 3538 3542 3546 3550 3554 3558 3562 3566 3570 3574 3578 3582 3586 3590 3594 3598 3602 3606 3610 3614 3618 3622 3626 3630 3634 3638 3642 3646 3650 3654 3658 3662 3666 3670 3674 3678 3682 3686 3690 3694 3698 3702 3706 3710 3714 3718 3722 3726 3730 3734 3738 3742 3746 3750 3754 3758 3762 3766 3770 3774 3778 3782 3786 3790 3794 3798 3802 3806 3810 3814 3818 3822 3826 3830 3834 3838 3842 3846 3850 3854 3858 3862 3866 3870 3874 3878 3882 3886 3890 3894 3898 3902 3906 3910 3914 3918 3922 3926 3930 3934 3938 3942 3946 3950 3954 3958 3962 3966 3970 3974 3978 3982 3986 3990 3994 3998 4002 4006 4010 4014 4018 4022 4026 4030 4034 4038 4042 4046 4050 4054 4058 4062 4066 4070 4074 4078 4082 4086 4090 4094 4098 4102 4106 4110 4114 4118 4122 4126 4130 4134 4138 4142 4146 4150 4154 4158 4162 4166 4170 4174 4178 4182 4186 4190 4194 4198 4202 4206 4210 4214 4218 4222 4226 4230 4234 4238 4242 4246 4250 4254 4258 4262 4266 4270 4274 4278 4282 4286 4290 4294 4298 4302 4306 4310 4314 4318 4322 4326 4330 4334 4338 4342 4346 4350 4354 4358 4362 4366 4370 4374 4378 4382 4386 4390 4394 4398 4402 4406 4410 4414 4418 4422 4426 4430 4434 4438 4442 4446 4450 4454 4458 4462 4466 4470 4474 4478 4482 4486 4490 4494 4498 4502 4506 4510 4514 4518 4522 4526 4530 4534 4538 4542 4546 4550 4554 4558 4562 4566 4570 4574 4578 4582 4586 4590 4594 4598 4602 4606 4610 4614 4618 4622 4626 4630 4634 4638 4642 4646 4650 4654 4658 4662 4666 4670 4674 4678 4682 4686 4690 4694 4698 4702 4706 4710 4714 4718 4722 4726 4730 4734 4738 4742 4746 4750 4754 4758 4762 4766 4770 4774 4778 4782 4786 4790 4794 4798 4802 4806 4810 4814 4818 4822 4826 4830 4834 4838 4842 4846 4850 4854 4858 4862 4866 4870 4874 4878 4882 4886 4890 4894 4898 4902 4906 4910 4914 4918 4922 4926 4930 4934 4938 4942 4946 4950 4954 4958 4962 4966 4970 4974 4978 4982 4986 4990 4994 4998 5002 5006 5010 5014 5018 5022 5026 5030 5034 5038 5042 5046 5050 5054 5058 5062 5066 5070 5074 5078 5082 5086 5090 5094 5098 5102 5106 5110 5114 5118 5122 5126 5130 5134 5138 5142 5146 5150 5154 5158 5162 5166 5170 5174 5178 5182 5186 5190 5194 5198 5202 5206 5210 5214 5218 5222 5226 5230 5234 5238 5242 5246 5250 5254 5258 5262 5266 5270 5274 5278 5282 5286 5290 5294 5298 5302 5306 5310 5314 5318 5322 5326 5330 5334 5338 5342 5346 5350 5354 5358 5362 5366 5370 5374 5378 5382 5386 5390 5394 5398 5402 5406 5410 5414 5418 5422 5426 5430 5434 5438 5442 5446 5450 5454 5458 5462 5466 5470 5474 5478 5482 5486 5490 5494 5498 5502 5506 5510 5514 5518 5522 5526 5530 5534 5538 5542 5546 5550 5554 5558 5562 5566 5570 5574 5578 5582 5586 5590 5594 5598 5602 5606 5610 5614 5618 5622 5626 5630 5634 5638 5642 5646 5650 5654 5658 5662 5666 5670 5674 5678 5682 5686 5690 5694 5698 5702 5706 5710 5714 5718 5722 5726 5730 5734 5738 5742 5746 5750 5754 5758 5762 5766 5770 5774 5778 5782 5786 5790 5794 5798 5802 5806 5810 5814 5818 5822 5826 5830 5834 5838 5842 5846 5850 5854 5858 5862 5866 5870 5874 5878 5882 5886 5890 5894 5898 5902 5906 5910 5914 5918 5922 5926 5930 5934 5938 5942 5946 5950 5954 5958 5962 5966 5970 5974 5978 5982 5986 5990 5994 5998 6002 6006 6010 6014 6018 6022 6026 6030 6034 6038 6042 6046 6050 6054 6058 6062 6066 6070 6074 6078 6082 6086 6090 6094 6098 6102 6106 6110 6114 6118 6122 6126 6130 6134 6138 6142 6146 6150 6154 6158 6162 6166 6170 6174 6178 6182 6186 6190 6194 6198 6202 6206 6210 6214 6218 6222 6226 6230 6234 6238 6242 6246 6250 6254 6258 6262 6266 6270 6274 6278 6282 6286 6290 6294 6298 6302 6306 6310 6314 6318 6322 6326 6330 6334 6338 6342 6346 6350 6354 6358 6362 6366 6370 6374 6378 6382 6386 6390 6394 6398 6402 6406 6410 6414 6418 6422 6426 6430 6434 6438 6442 6446 6450 6454 6458 6462 6466 6470 6474 6478 6482 6486 6490 6494 6498 6502 6506 6510 6514 6518 6522 6526 6530 6534 6538 6542 6546 6550 6554 6558 6562 6566 6570 6574 6578 6582 6586 6590 6594 6598 6602 6606 6610 6614 6618 6622 6626 6630 6634 6638 6642 6646 6650 6654 6658 6662 6666 6670 6674 6678 6682 6686 6690 6694 6698 6702 6706 6710 6714 6718 6722 6726 6730 6734 6738 6742 6746 6750 6754 6758 6762 6766 6770 6774 6778 6782 6786 6790 6794 6798 6802 6806 6810 6814 6818 6822 6826 6830 6834 6838 6842 6846 6850 6854 6858 6862 6866 6870 6874 6878 6882 6886 6890 6894 6898 6902 6906 6910 6914 6918 6922 6926 6930 6934 6938 6942 6946 6950 6954 6958 6962 6966 6970 6974 6978 6982 6986 6990 6994 6998 7002 7006 7010 7014 7018 7022 7026 7030 7034 7038 7042 7046 7050 7054 7058 7062 7066 7070 7074 7078 7082 7086 7090 7094 7098 7102 7106 7110 7114 7118 7122 7126 7130 7134 7138 7142 7146 7150 7154 7158 7162 7166 7170 7174 7178 7182 7186 7190 7194 7198 7202 7206 7210 7214 7218 7222 7226 7230 7234 7238 7242 7246 7250 7254 7258 7262 7266 7270 7274 7278 7282 7286 7290 7294 7298 7302 7306 7310 7314 7318 7322 7326 7330 7334 7338 7342 7346 7350 7354 7358 7362 7366 7370 7374 7378 7382 7386 7390 7394 7398 7402 7406 7410 7414 7418 7422 7426 7430 7434 7438 7442 7446 7450 7454 7458 7462 7466 7470 7474 7478 7482 7486 7490 7494 7498 7502 7506 7510 7514 7518 7522 7526 7530 7534 7538 7542 7546 7550 7554 7558 7562 7566 7570 7574 7578 7582 7586 7590 7594 7598 7602 7606 7610 7614 7618 7622 7626 7630 7634 7638 7642 7646 7650 7654 7658 7662 7666 7670 7674 7678 7682 7686 7690 7694 7698 7702 7706 7710 7714 7718 7722 7726 7730 7734 7738 7742 7746 7750 7754 7758 7762 7766 7770 7774 7778 7782 7786 7790 7794 7798 7802 7806 7810 7814 7818 7822 7826 7830 7834 7838 7842 7846 7850 7854 7858 7862 7866 7870 7874 7878 7882 7886 7890 7894 7898 7902 7906 7910 7914 7918 7922 7926 7930 7934 7938 7942 7946 7950 7954 7958 7962 7966 7970 7974 7978 7982 7986 7990 7994 7998 8002 8006 8010 8014 8018 8022 8026 8030 8034 8038 8042 8046 8050 8054 8058 8062 8066 8070 8074 8078 8082 8086 8090 8094 8098 8102 8106 8110 8114 8118 8122 8126 8130 8134 8138 8142 8146 8150 8154 8158 8162 8166 8170 8174 8178 8182 8186 8190 8194 8198 8202 8206 8210 8214 8218 8222 8226 8230 8234 8238 8242 8246 8250 8254 8258 8262 8266 8270 8274 8278 8282 8286 8290 8294 8298 8302 8306 8310 8314 8318 8322 8326 8330 8334 8338 8342 8346 8350 8354 8358 8362 8366 8370 8374 8378 8382 8386 8390 8394 8398 8402 8406 8410 8414 8418 8422 8426 8430 8434 8438 8442 8446 8450 8454 8458 8462 8466 8470 8474 8478 8482 8486 8490 8494 8498 8502 8506 8510 8514 8518 8522 8526 8530 8534 8538 8542 8546 8550 8554 8558 8562 8566 8570 8574 8578 8582 8586 8590 8594 8598 8602 8606 8610 8614 8618 8622 8626 8630 8634 8638 8642 8646 8650 8654 8658 8662 8666 8670 8674 8678 8682 8686 8690 8694 8698 8702 8706 8710 8714 8718 8722 8726 8730 8734 8738 8742 8746 8750 8754 8758 8762 8766 8770 8774 8778 8782 8786 8790 8794 8798 8802 8806 8810 8814 8818 8822 8826 8830 8834 8838 8842 8846 8850 8854 8858 8862 8866 8870 8874 8878 8882 8886 8890 8894 8898 8902 8906 8910 8914 8918 8922 8926 8930 8934 8938 8942 8946 8950 8954 8958 8962 8966 8970 8974 8978 8982 8986 8990 8994 8998 9002 9006 9010 9014 9018 9022 9026 9030 9034 9038 9042 9046 9050 9054 9058 9062 9066 9070 9074 9078 9082 9086 9090 9094 9098 9102 9106 9110 9114 9118 9122 9126 9130 9134 9138 9142 9146 9150 9154 9158 9162 9166 9170 9174 9178 9182 9186 9190 9194 9198 9202 9206 9210 9214 9218 9222 9226 9230 9234 9238 9242 9246 9250 9254 9258 9262 9266 9270 9274 9278 9282 9286 9290 9294 9298 9302 9306 9310 9314 9318 9322 9326 9330 9334 9338 9342 9346 9350 9354 9358 9362 9366 9370 9374 9378 9382 9386 9390 9394 9398 9402 9406 9410 9414 9418 9422 9426 9430 9434 9438 9442 9446 9450 9454 9458 9462 9466 9470 9474 9478 9482 9486 9490 9494 9498 9502 9506 9510 9514 9518 9522 9526 9530 9534 9538 9542 9546 9550 9554 9558 9562 9566 9570 9574 9578 9582 9586 9590 9594 9598 9602 9606 9610 9614 9618 9622 9626 9630 9634 9638 9642 9646 9650 9654 9658 9662 9666 9670 9674 9678 9682 9686 9690 9694 9698 9702 9706 9710 9714 9718 9722 9726 9730 9734 9738 9742 9746 9750 9754 9758 9762 9766 9770 9774 9778 9782 9786 9790 9794 9798 9802 9806 9810 9814 9818 9822 9826 9830 9834 9838 9842 9846 9850 9854 9858 9862 9866 9870 9874 9878 9882 9886 9890 9894 9898 9902 9906 9910 9914 9918 9922 9926 9930 9934 9938 9942 9946 9950 9954 9958 9962 9966 9970 9974 9978 9982 9986 9990 9994 9998

1764 1778 1782 1786 1790 1794 1798 1802 1806 1810 1814 1818 1822 1826 1830 1834 1838 1842 1846 1850 1854 1858 1862 1866 1870 1874 1878 1882 1886 1890 1894 1898 1902 1906 1910 1914 1918 1922 1926 1930 1934 1938 1942 1946 1950 1954 1958 1962 1966 1970 1974 1978 1982 1986 1990 1994 1998 2002 2006 2010 2014 2018 2022 2026 2030 2034 2038 2042 2046 2050 2054 2058 2062 2066 2070 2074 2078 2082 2086 2090 2094 2098 2102 2106 2110 2114 2118 2122 2126 2130 2134 2138 2142 2146 2150 2154 2158 2162 2166 2170 2174 2178 2182 2186 2190 2194 2198 2202 2206 2210 2214 2218 2222 2226 2230 2234 2238 2242 2246 2250 2254 2258 2262 2266 2270 2274 2278 2282 2286 2290 2294 2298 2302 2306 2310 2314 2318 2322 2326 2330 2334 2338 2342 2346 2350 2354 2358 2362 2366 2370 2374 2378 2382 2386 2390 2394 2398 2402 2406 2410 2414 2418 2422 2426 2430 2434 2438 2442 2446 2450 2454 2458 2462 2466 2470 2474 2478 2482 2486 2490 2494 2498 2502 2506 2510 2514 2518 2522 2526 2530 2534 2538 2542 2546 2550

**CHIMINATIVE AREA = 7,7859 MI**

HYDROGRAPH AT STATION A1  
PLAN 1. RATIO = 0.50 A1

DA	MN	HRMN	ORD	FLOW	DA	MN	HRMN	ORD	FLOW	DA	MN	HRMN	ORD	FLOW
0115	76	23			0120	151	506	226		0125	152	570	228	
0625	76	24			0630	152	611	228		0635	153	675	228	
0635	76	25			0640	153	643	229		0645	154	724	229	
0645	76	26			0650	154	754	229		0655	155	816	229	
0655	76	27			0700	155	816	229		0705	156	893	229	
0705	76	28			0710	156	907	229		0715	157	981	229	
0715	76	29			0720	157	981	229		0725	158	1031	229	
0725	76	30			0730	158	1031	229		0735	159	1086	229	
0735	76	31			0740	159	1086	229		0745	160	1140	229	
0745	76	32			0750	160	1140	229		0755	161	1193	229	
0755	76	33			0800	161	1193	229		0805	162	1243	229	
0805	76	34			0810	162	1243	229		0815	163	1293	229	
0815	76	35			0820	163	1293	229		0825	164	1343	229	
0825	76	36			0830	164	1343	229		0835	165	1393	229	
0835	76	37			0840	165	1393	229		0845	166	1443	229	
0845	76	38			0850	166	1443	229		0855	167	1493	229	
0855	76	39			0900	167	1493	229		0905	168	1543	229	
0905	76	40			0910	168	1543	229		0915	169	1593	229	
0915	76	41			0920	169	1593	229		0925	170	1643	229	
0925	76	42			0930	170	1643	229		0935	171	1693	229	
0935	76	43			0940	171	1693	229		0945	172	1743	229	
0945	76	44			0950	172	1743	229		0955	173	1793	229	
0955	76	45			1000	173	1793	229		1005	174	1843	229	
1005	76	46			1010	174	1843	229		1015	175	1893	229	
1015	76	47			1020	175	1893	229		1025	176	1943	229	
1025	76	48			1030	176	1943	229		1035	177	1993	229	
1035	76	49			1040	177	1993	229		1045	178	2043	229	
1045	76	50			1050	178	2043	229		1055	179	2093	229	
1055	76	51			1060	179	2093	229		1065	180	2143	229	
1065	76	52			1070	180	2143	229		1075	181	2193	229	
1075	76	53			1080	181	2193	229		1085	182	2243	229	
1085	76	54			1090	182	2243	229		1095	183	2293	229	
1095	76	55			1100	183	2293	229		1105	184	2343	229	
1105	76	56			1110	184	2343	229		1115	185	2393	229	
1115	76	57			1120	185	2393	229		1125	186	2443	229	
1125	76	58			1130	186	2443	229		1135	187	2493	229	
1135	76	59			1140	187	2493	229		1145	188	2543	229	
1145	76	60			1150	188	2543	229		1155	189	2593	229	
1155	76	61			1160	189	2593	229		1165	190	2643	229	
1165	76	62			1170	190	2643	229		1175	191	2693	229	
1175	76	63			1180	191	2693	229		1185	192	2743	229	
1185	76	64			1190	192	2743	229		1195	193	2793	229	
1195	76	65			1200	193	2793	229		1205	194	2843	229	
1205	76	66			1210	194	2843	229		1215	195	2893	229	
1215	76	67			1220	195	2893	229		1225	196	2943	229	
1225	76	68			1230	196	2943	229		1235	197	2993	229	
1235	76	69			1240	197	2993	229		1245	198	3043	229	
1245	76	70			1250	198	3043	229		1255	199	3093	229	
1255	76	71			1260	199	3093	229		1265	200	3143	229	
1265	76	72			1270	200	3143	229		1275	201	3193	229	
1275	76	73			1280	201	3193	229		1285	202	3243	229	
1285	76	74			1290	202	3243	229		1295	203	3293	229	
1295	76	75			1300	203	3293	229		1305	204	3343	229	
1305	76	76			1310	204	3343	229		1315	205	3393	229	
1315	76	77			1320	205	3393	229		1325	206	3443	229	
1325	76	78			1330	206	3443	229		1335	207	3493	229	
1335	76	79			1340	207	3493	229		1345	208	3543	229	
1345	76	80			1350	208	3543	229		1355	209	3593	229	
1355	76	81			1360	209	3593	229		1365	210	3643	229	
1365	76	82			1370	210	3643	229		1375	211	3693	229	
1375	76	83			1380	211	3693	229		1385	212	3743	229	
1385	76	84			1390	212	3743	229		1395	213	3793	229	
1395	76	85			1400	213	3793	229		1405	214	3843	229	
1405	76	86			1410	214	3843	229		1415	215	3893	229	
1415	76	87			1420	215	3893	229		1425	216	3943	229	
1425	76	88			1430	216	3943	229		1435	217	3993	229	
1435	76	89			1440	217	3993	229		1445	218	4043	229	
1445	76	90			1450	218	4043	229		1455	219	4093	229	
1455	76	91			1460	219	4093	229		1465	220	4143	229	
1465	76	92			1470	220	4143	229		1475	221	4193	229	
1475	76	93			1480	221	4193	229		1485	222	4243	229	
1485	76	94			1490	222	4243	229		1495	223	4293	229	
1495	76	95			1500	223	4293	229		1505	224	4343	229	
1505	76	96			1510	224	4343	229		1515	225	4393	229	
1515	76	97			1520	225	4393	229		1525	226	4443	229	
1525	76	98			1530	226	4443	229		1535	227	4493	229	
1535	76	99			1540	227	4493	229		1545	228	4543	229	
1545	76	100			1550	228	4543	229		1555	229	4593	229	
1555	76	101			1560	229	4593	229		1565	230	4643	229	
1565	76	102			1570	230	4643	229		1575	231	4693	229	
1575	76	103			1580	231	4693	229		1585	232	4743	229	
1585	76	104			1590	232	4743	229		1595	233	4793	229	
1595	76	105			1600	233	4793	229		1605	234	4843	229	
1605	76	106			1610	234	4843	229		1615	235	4893	229	
1615	76	107			1620	235	4893	229		1625	236	4943	229	
1625	76	108			1630	236	4943	229		1635	237	4993	229	
1635	76	109			1640	237	4993	229		1645	238	5043	229	
1645	76	110			1650	238	5043	229		1655	239	5093	229	
1655	76	111			1660	239	5093	229		1665	240	5143	229	
1665	76	112			1670	240	5143	229		1675	241	5193	229	
1675	76	113			1680	241	5193	229		1685	242	5243	229	
1685	76	114			1690	242	5243	229		1695	243	5293	229	
1695	76	115			1700	243	5293	229		1705	244	5343	229	
1705	76	116			1710	244	5343	229		1715	245	5393	229	
1715	76	117			1720	245	5393	229		1725	246	5443	229	
1725	76	118			1730	246	5443	229		1735	247	5493	229	
1735	76	119			1740	247	5493	229		1745	248	5543	229	
1745	76	120			1750	248	5543</							

MAXIMUM AVE 24-HR	22.29	10.4765	7.70 SO MI
CUMULATIVE AREA "			
TIME (HRS)	{CFS}	b-hr	
16.92	{INCHES}	66.95	
	{AC-FT}	33.07	
		33.07	

14 KK

## ROUTE INFLOW HYDROGRAPH THROUGH HOPE LAKE

4.2

## HYDROGRAPH ROUTING DATA

IS RS	STORAGE ROUTING ISIPS ATIP ASVRI	STOK 64.00 WORKING R AND D COEFFICIENT	NUMBER OF SUBREACHES TYPE OF INITIAL CONDITION			
16 SV	STORAGE 0.0	64.0 70.0	100.0	150.0	160.0	210.0 350.0 520.0 650.0
17 SE	ELEVATION 417.40	424.70 425.20	426.00	426.70 427.20	427.70 428.70	430.00 432.00
18 SO	DISCHARGE 0.	0. 57.	337.	846. 1464.	2168. 4133.	7442. 13216.
19 SE	ELEVATION 417.40	424.70 425.20	426.00	426.70 427.20	427.70 428.70	430.00 432.00
20 SS	SPILLWAY CREL SPWD CCAN EXPW	424.70 60.00 62.70 1.50	SPILLWAY CREST ELEVATION SPILLWAY WIDTH WEIR COEFFICIENT EXponent OF HEAD			
21 ST	TOP OF DAM TOPEL OHWIO COPO EXPO	426.00 173.00 0.0 1.50	ELEVATION AT TOP OF DAM DAM WIDTH WEIR COEFFICIENT EXponent OF HEAD	***		
			COMPUTED STORAGE-OUTFLOW CURVE 100.00 150.00	210.00 350.00 520.00 650.00		
	STORAGE 0.0	64.00	70.00	1664.00 2168.00	4133.00 7442.00	13216.00
	OUTFLOW 0.0	0.0	57.00	337.00		

HYDROGRAPH AT STATION A2  
PLAN 1. RAILING NO. 10

MON	HHRN	GRC	OUTFLOW	STORAGE	DA		MON		HHRN		GRC		OUTFLOW	STORAGE	DA		MON		HHRN		GRC	
					STAGE	DA	STAGE	DA	STAGE	DA	STAGE	DA			STAGE	DA	STAGE	DA	STAGE	DA		
6600	0100	0100	0100	0100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6605	0105	0105	0105	0105	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6610	0110	0110	0110	0110	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6615	0115	0115	0115	0115	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6620	0120	0120	0120	0120	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6625	0125	0125	0125	0125	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6630	0130	0130	0130	0130	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6635	0135	0135	0135	0135	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6640	0140	0140	0140	0140	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6645	0145	0145	0145	0145	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6650	0150	0150	0150	0150	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6655	0155	0155	0155	0155	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6660	0200	0200	0200	0200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6665	0205	0205	0205	0205	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6670	0210	0210	0210	0210	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6675	0215	0215	0215	0215	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6680	0220	0220	0220	0220	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6685	0225	0225	0225	0225	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6690	0230	0230	0230	0230	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6695	0235	0235	0235	0235	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6700	0240	0240	0240	0240	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6705	0245	0245	0245	0245	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6710	0250	0250	0250	0250	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6715	0255	0255	0255	0255	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6720	0300	0300	0300	0300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6725	0305	0305	0305	0305	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6730	0310	0310	0310	0310	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6735	0315	0315	0315	0315	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6740	0320	0320	0320	0320	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6745	0325	0325	0325	0325	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6750	0330	0330	0330	0330	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6755	0335	0335	0335	0335	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6760	0340	0340	0340	0340	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6765	0345	0345	0345	0345	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6770	0350	0350	0350	0350	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6775	0355	0355	0355	0355	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6780	0360	0360	0360	0360	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6785	0365	0365	0365	0365	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6790	0370	0370	0370	0370	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6795	0375	0375	0375	0375	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6800	0380	0380	0380	0380	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6805	0385	0385	0385	0385	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6810	0390	0390	0390	0390	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6815	0395	0395	0395	0395	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6820	0400	0400	0400	0400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6825	0405	0405	0405	0405	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6830	0410	0410	0410	0410	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6835	0415	0415	0415	0415	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6840	0420	0420	0420	0420	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6845	0425	0425	0425	0425	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6850	0430	0430	0430	0430	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6855	0435	0435	0435	0435	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6860	0440	0440	0440	0440	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6865	0445	0445	0445	0445	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6870	0450	0450	0450	0450	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6875	0455	0455	0455	0455	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6880	0500	0500	0500	0500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6885	0505	0505	0505	0505	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6890	0510	0510	0510	0510	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6895	0515	0515	0515	0515	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6900	0520	0520	0520	0520	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6905	0525	0525	0525	0525	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6910	0530	0530	0530	0530	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6915	0535	0535	0535	0535	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6920	0540	0540	0540	0540	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6925	0545	0545	0545	0545	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6930	0550	0550	0550	0550	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6935	0555	0555	0555	0555	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6940	0600	0600	0600	0600	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6945	0605	0605	0605	0605	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6950	0610	0610	0610	0610	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6955	0615	0615	0615	0615																		

THE HISTORY OF THE AMERICAN PEOPLE

PEAK FLOW (CFS)	TIME (HR)	TIME (CFS)	TIME (CFS)	MAXIMUM AVERAGE FLOW 24-HR	MAXIMUM AVERAGE FLOW 72-HR
19.0	19.0	19.0	19.0	2.69	2.69

STAGE (AC-F1)	TIME (hr.)	STAGE AC-F1	TIME (hr.)	STAGE AC-F2	TIME (hr.)
57.	19.50	1145	0-1HR	MAXIMUM AVERAGE STORAGE	24.92-HR
57.	19.50	1145	474.	24-HR	202.

CUMULATIVE AHTA = 7.70 SC MI

PEAK FLOW AND STAGE (LIND-UF-PERIGO) SUMMARY FOR MULTIPLE PLANT RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND; AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

LOCATION	STATION	AREA	PLAN	RATIO 1	RATIO 2	RATIO 3
HYDROGRAPH AT	A1	7.70	1	Flow	0.10	0.25
ROUTED TO	A2	7.70	1	Flow	16.82	16.44
				** PEAK STAGES IN FEET	87.28	87.92
			1	STAGE	27.36	28.67
				TIME	19.32	19.50
					430.33	430.33

## SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION

A2

PLAN	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP UF CAM		
1	424.70 69. 0.	424.70 64. 0.	424.70 64. 0.	426.00 100. 337.		
RATIO OF FHF TO M.S.ELEV	MAXIMUM RESERVOIR DEPTH OVER DAM	MAXIMUM STORAGE ACFT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF OUTFLOW MAX HOURS	TIME OF FAILURE HOURS
6.10	427.36	1.36	190.	9.42	19.42	0.0
0.25	426.99	2.09	398.	8.07	19.67	0.0
0.50	430.93	4.93	574.	8.85	13.25	19.50

\*\* NORMAL END OF JOB \*\*

**APPENDIX 5**  
**REFERENCES**

**HOPE LAKE DAM**

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**REFERENCES**

**HOPE LAKE DAM**

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